### BHARAT INSTITUTE OF ENGGINEERING AND TECHNOLOGY

## (APPROVED BY AICTE AFFILIATED TO SCTE & VT)

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PIN- 760002



## LECTURE NOTES

ON

STRUCTURAL MECHANICS

CIVIL, 3<sup>RD</sup> SEMESTER

PREPARED BY

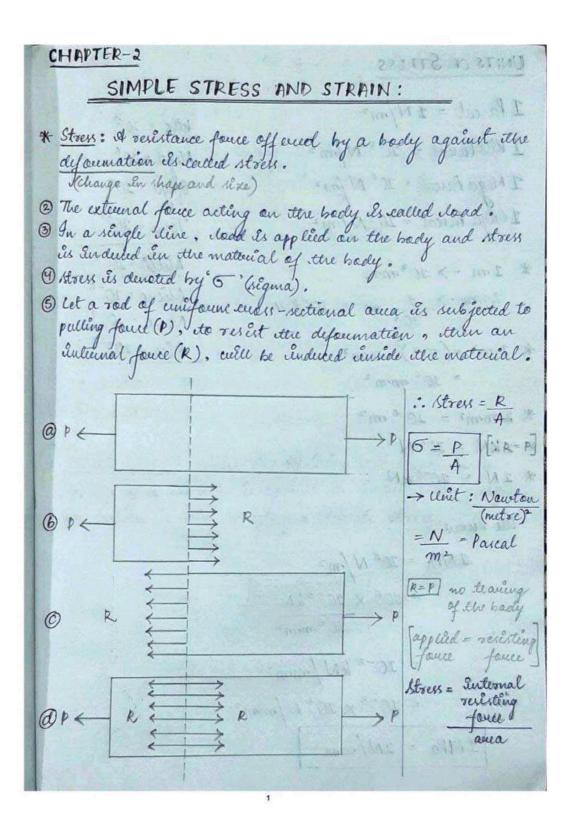
BIPIN KUMAR TRIPATHY

DEPARTMENT OF CIVIL ENGINEERING

BIET, MOHADA, BERHAMPUR

## Chapter 1

## SIMPLE AND COMPLEX STRESS AND STRAIN.



## UNITS OF STRESS

$$*1m \rightarrow 10^3 mm$$

$$2mm \rightarrow 1 m = 10^{-3} m$$

$$* 1m^2 = (10^3)^2 mm^2$$

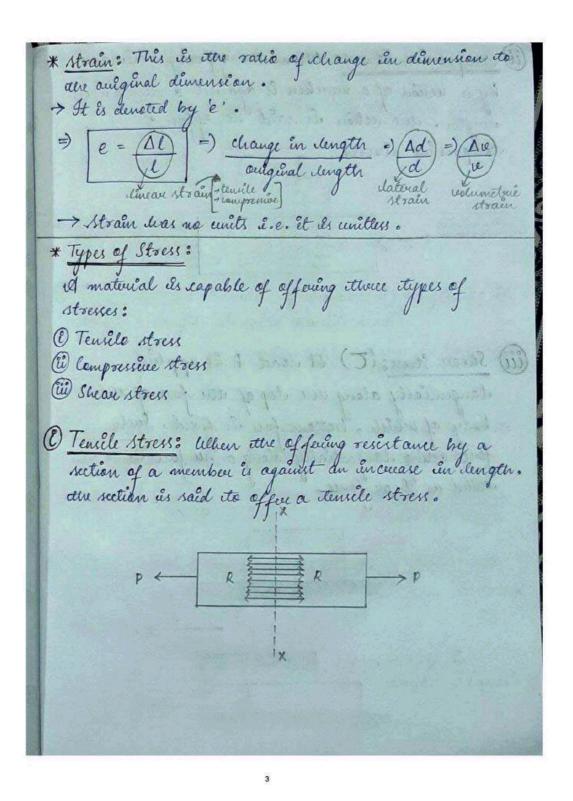
ale know,

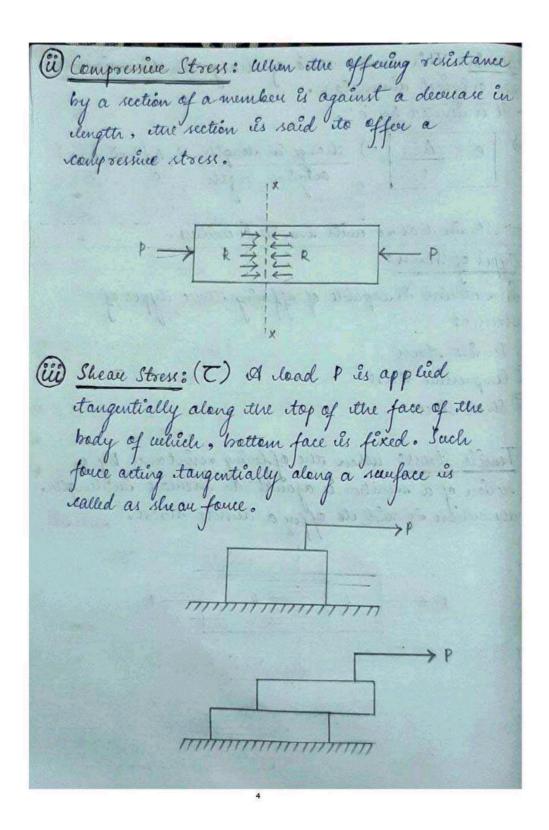
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SIMILE STREETS UND STREET

$$\text{Nülli} = 10^{-3}$$

$$p_{ico} = 10^{-12}$$

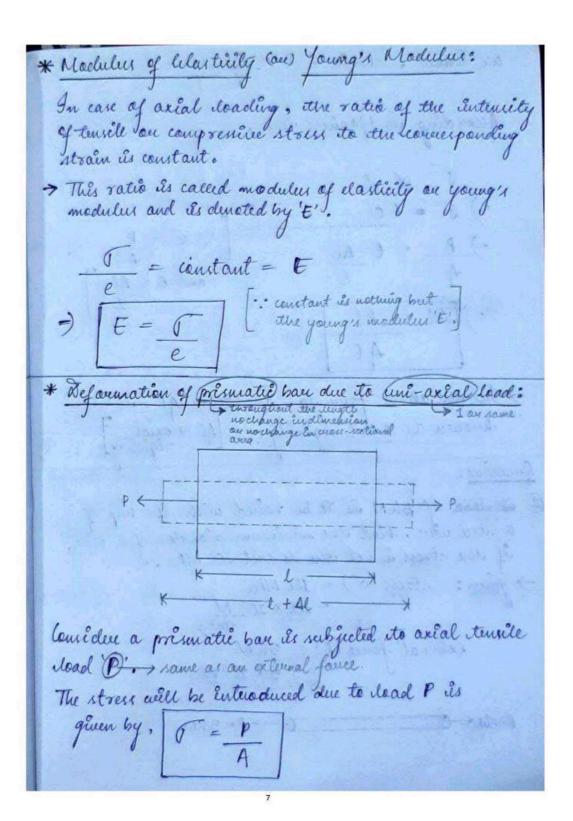




-> The resistance provided in this case is ealled shear resestance. -> Shear stress is defined as the ratio of shear resistance ito ille shear anca. mathematically, T = R 01.11.2021 \* Types of strain: Strain can be of 4 types: (1) Tensile strain: The ratio of increase in length to its acciginal length, is salled tensile strain. l = <u>Al</u> → here, Al → change un Incuease in (i) Compressive Strain: The ratio of decrease in length to the original length, is called compressive strain. l = Al → hun, Al → change in dernease (ii) Lateral strain: The ratio of the change in lateral dimension its the original clateral dimension, is called date al strain. e = Ad | -> here, Ad -> change ûn datedal d'émension ( Molunetric strain: The ratio of the change in volume do ilt oniginal volume, is called as volumetric strain. e = Au -> hun. Au -> change ûn \* Hoche is Law: (most imp) It states that " when a material is do aded such that the intensity of stress within a curtain climit, the ratio of the intensity of the stress to the socresponding strain is a constant." stress = 5 = constant. strain =) \_ = constant =) o = constant x e σαe

-> It also can be stated as "Stress as directly

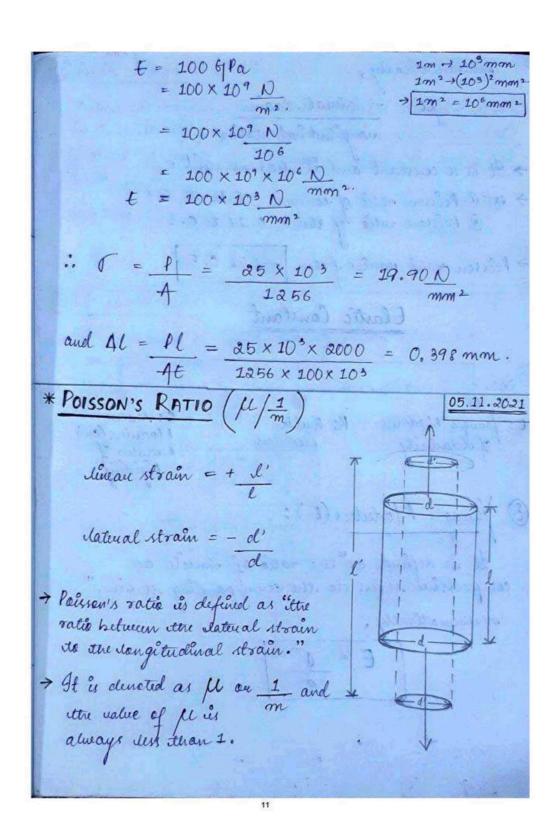
proportional do strain, within a centain light."

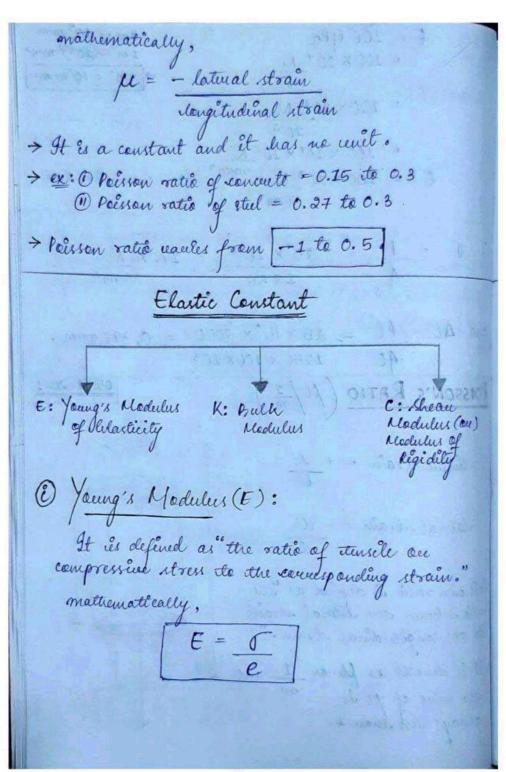


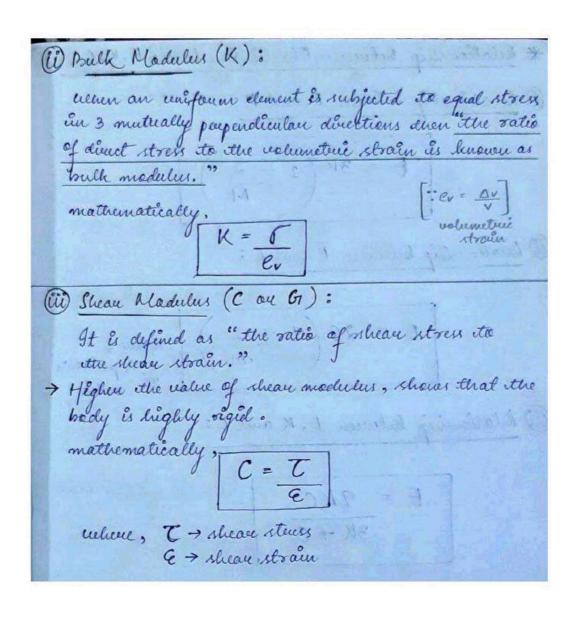
une lemon , strain : e = Dl According to Hacke's clave, -> In the above foundla, the teum At' is huoven as axial rigidity. At rigidity Questions: 1 A load of 5kN is to be raised with the help of a steel where. Find the minimum diameter of a wive. if the stress is not the to exit 100 MPa. I if the stress as (5) = 100 MPa  $\Rightarrow 9 \frac{\text{men}}{\text{m}^2}$ :  $stress (5) = 100 \times 10^6 \frac{\text{N}}{\text{m}^2}$ external force (1) = 5kN=  $5 \times 10^3 N$ → P-5kN PESLUX 6

: 
$$\Delta l = Pl = 300 \times 10^{5} \times 500 = 3.75 \text{ mm}$$

At  $= 200 \times 200 \times 200 \times 200 \times 2000 \times 20000 \times 2000$ 







\* Relationship between Elastic Constants E, K, C:

(i) Relationship between E and K:

$$E = 3K \left(1 - \frac{2}{M}\right)$$

(ii) Relationship between E and C:

$$E = 2C \left(1 + \frac{1}{m}\right) \quad \text{where}; \quad \text{ article is pressent, ratio}$$

(iii) Relationship between E, K and C:

$$E = 9KC \quad 3K + C$$

\* Proof: 
$$E = \frac{9KC}{3K+C}$$

we know,

 $E = 3K\left(1 - \frac{2}{M}\right) = 1 - \frac{2}{M} = \frac{E}{3K}$ 
 $E = 2C\left(1 + \frac{1}{M}\right) = 1 + \frac{1}{m} = \frac{E}{2C}$ 

multiplying a sin eqn 2

 $2\left(1 + \frac{1}{M}\right) = 2\left(\frac{E}{2C}\right)$ 
 $2\left(1 + \frac{1}{M}\right) = 2\left(\frac{E}{2C}\right)$ 

now adding and 3

 $1 - \frac{2}{M} + 2 + \frac{2}{M} = \frac{E}{3K} + \frac{E}{C}$ 
 $1 + 2 = \frac{E}{3K} + \frac{E}{C}$ 
 $3\left(3KC\right) = EC + E3K$ 
 $3\left(3KC\right) = EC + E3K$ 

$$=) \begin{array}{c} 9KC = E(C+3K) \\ =) \overline{E} = \frac{9KC}{3K+C} \end{array} \quad \text{hence proved}$$

$$\overline{Saustiens:}$$

$$\boxed{3 \text{ The modulus of rigidity of a matinial is}} \\ 0.8 \times 10^5 \, N \quad \text{. Fill titl poissons ratio if title} \\ \overline{mm} \\ \overline{modulus of elasticity of that matinial is a.1 \times 10^5 \, N \\ \overline{mm}^2 \\ E = 2.1 \times 10^5 \, N \\ \overline{mm}^2 \\ E = 2.1 \times 10^5 \, N \\ \overline{mm}^2 \\ \hline =) \begin{array}{c} 2.1 \times 10^5 \, N \\ \overline{mm}^2 \\ \hline = 2.1 \times 10^5 \, N \\ \overline{mm}^2 \\ \overline{mm}^2$$

Paison's valie:

$$\frac{1}{M} = \frac{latural \ dvain}{langituduial \ stain}$$
=)  $\frac{1}{M} = \frac{0.00015}{100} \times E$ 
=)  $\frac{1}{M} = \frac{0.00015}{100} \times E$ 
=)  $\frac{1}{EM} = \frac{0.00015}{100}$ 
=)  $ME = \frac{100}{0.00015}$ 
=)  $ME = \frac{100}{3}$ 

we have,  $E = 2C \cdot (1 + \frac{1}{M})$ 
=)  $ME = 2C \cdot (M+1)$ 
=)  $ME = 2X \cdot 0.8 \times 10^{5} (M+1)$ 
=)  $ME = 2X \cdot 0.8 \times 10^{5} (M+1)$ 
=)  $2X \cdot 0.8 \times 10^{5} (M+1) = \frac{1}{3}$ 

-) 
$$M + 1 = \frac{2 \times 10^6}{3(2 \times 0.8 \times 10^5)}$$

=)  $M = \frac{2 \times 10^6}{3(2 \times 0.8 \times 10^5)}$ 

=)  $M = \frac{1}{3.167}$ 
 $\therefore \mu = \frac{1}{M} = \frac{1}{3.167}$ 
 $\therefore E = 2 \times (1 + \frac{1}{M})$ 

=)  $E = 2 \times 0.8 \times 10^5 (1 + 0.315)$ 

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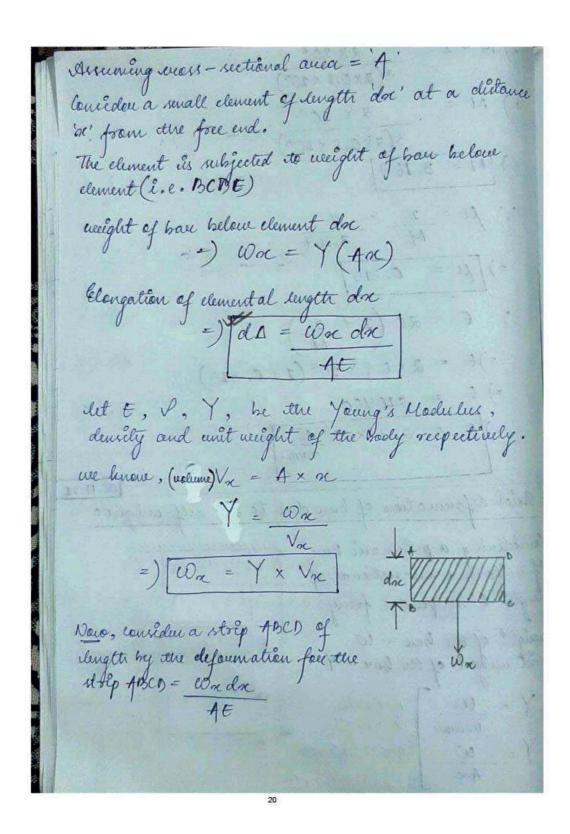
=)  $E = 2 \times 0.8 \times 10^5 (1 + 0.315)$ 

=)  $E = 2 \times 0.8 \times 10^5 (1 + 0.315)$ 

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=)  $E = 2 \times 0.8 \times 10^5 (1 + 0$ 



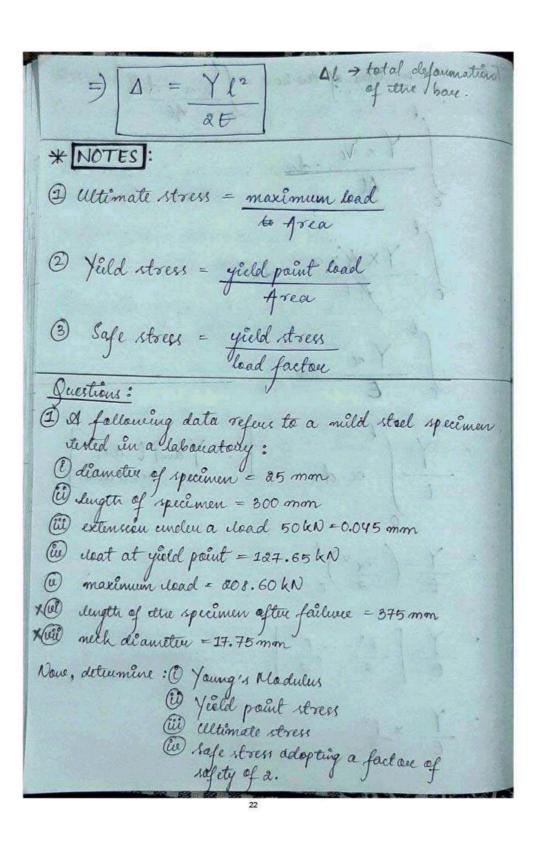
Total defaumation of the base = 
$$\int_{0}^{L} \frac{u_{n} \times dx}{4t}$$

=  $\int_{0}^{L} \frac{1}{4t} \times \frac{1}{4t} dx$ 

=  $\int_{0}^{L} \frac{1}{4t} \times \frac{1}{4t} dx$ 

=  $\int_{0}^{L} \frac{1}{4t} \times \frac{1}{4t} dx$ 

=  $\int_{0}^{L} \frac{1}{4t} dx = \int_{0}^{L} \frac{1}{4t} dx$ 



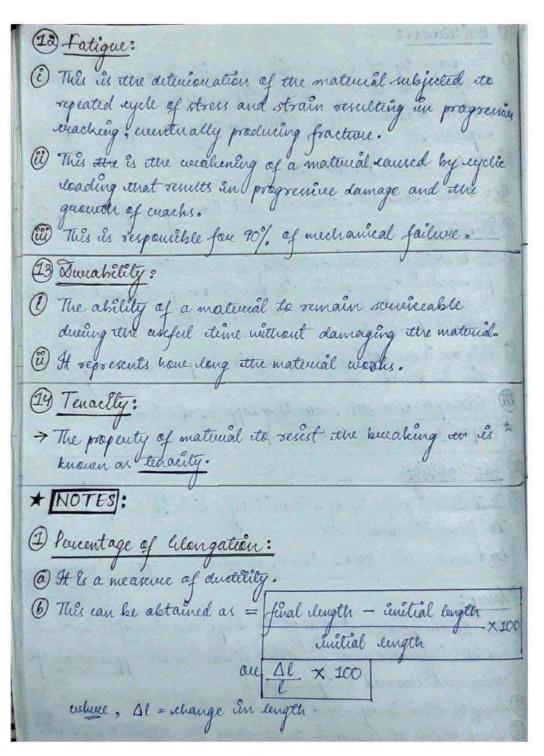
```
> gueen: d = 25 mm
            = 300 mm
           P = 50 kN
            = 50×103 N
          Al = 0.045 mm
 yield point load = 127.65 kN = 127.65 × 103 N
  maximum daad = 208.60 kN
             = 208.60 × 103 N
  cload factore = 2.
( Al = Pl
 =) E = Pl
AAL
 =) E =
```

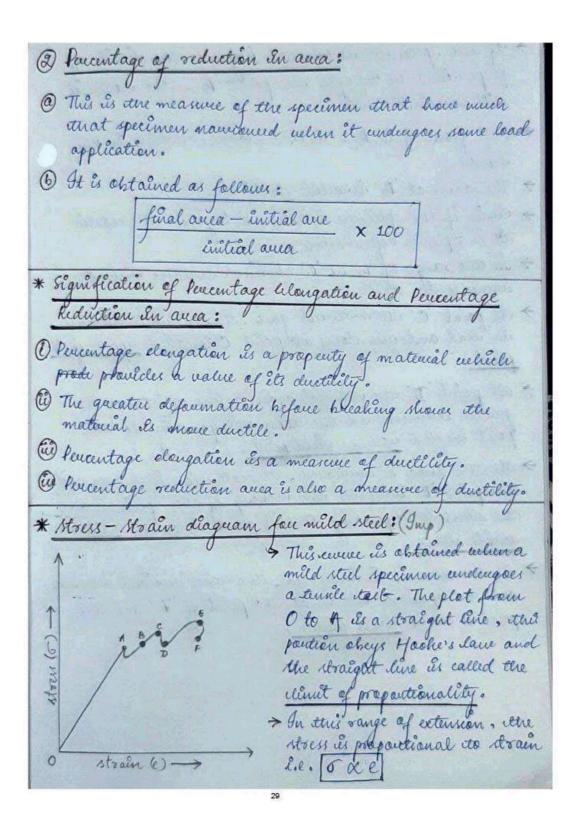
# Mechanical Properties Of Materials

## MECHANICAL PROPERTIES OF MATERIALS: 1 Rigidity: 1 This its defined as the property passessed by a solid body to change lits shape. (1) It means when an exturnal fouce its applied to the solid material, there went be any change in its shape che to ilutumolecular attraction by tent-closely packed particles. (ii) This is the property of the material to resistance the bending. (2) blasticity: 1 This is the property of a body by wirtue of which in return its original shape after remobal of external force causing deformation which its applied on it. (i) Elastic property entirely depends upon the type of material and not an the shape and size. 3 Plasticity: 1 This is the ability of a solid material to undergo purmanent defoumation whethe force is applied to it. (1) The ability of a material to retain the changed shape under application of load is known as plasticity (iii) Plastic deformation is the property of ductile and malleable solids. v

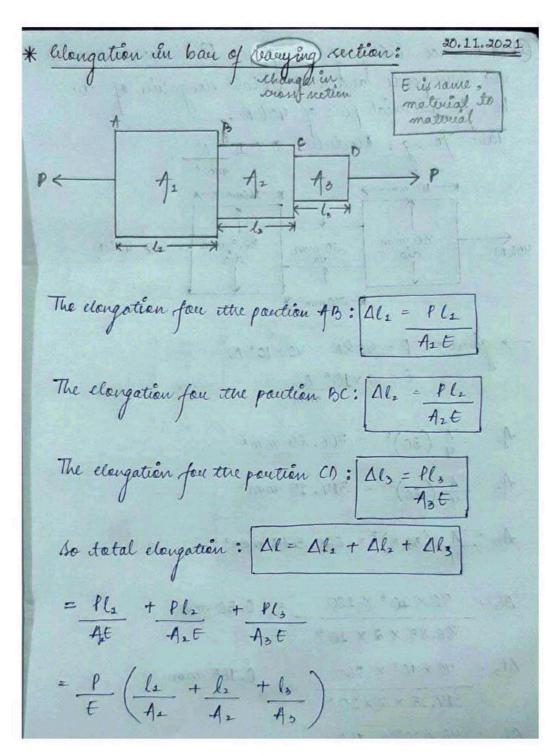
(4) Lempressibility: 2月1日 以至日 7月1 1 This is the property of material by wirtue of which il tends to flatter and reduce in stre unelew pressure. (i) This nature on property of material changes the intermolecular structure of the material. (5) Handness: 1 The property of material by wenter of which it resists the local seveface defounation when undergoes obrasion dulling, impact, etc. (ii) It is the state of material, being hand for which it can withstand friction 6 Toughness: 1 The aucunt of energy par unit wolume that a material can absorb before suptime is called taughness, W It can be defined as the ability of a matural to resest bushing when fouce is applied to it. (ii) This property allows the material its deform before rupture de fractime. 7 Stiffness: 1 The property of material acticle resists deformation when a faire is applied ito it. This is the rigidity of a nonterial. (ii) The material having more flexibility has less stiffners. (iii) A stiff material has high doing modules.

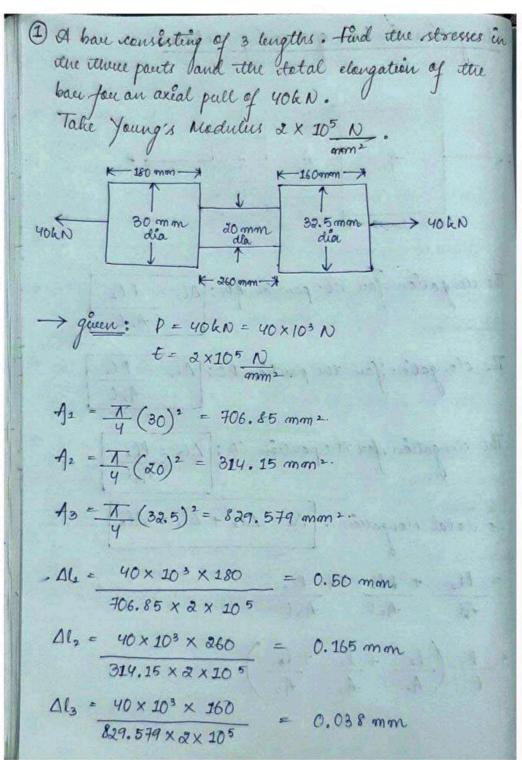
(8) Brittleness: 1 The property of a material by which it fractives when subjected to stress without affournation. @ writtle material has a little itendency to deform before ouptivece. (ii) It has small plastic region. le: brone, concuett, cenamic, cast bron, glass products, etc. @ Ductility: 1 It is defined as the ability of a material to undergo permandent deformation terrough clargation and reduction incress-sectional area are bending at some temperature without fractiving. @ This on is an ability to undergo last permanent deformaition in tuccon . lexample of dutile material + eapper, aluminium, steel. \* apposite to ductile is bentle 10 Malleability: ( This is the property of material by which it can be beaten to four its their shots . lex! lead, tin, gold, selver, aluminium, copper, eron 11) lucep: This is the permanent change in shape and sixe of a material which increases as a function of time under application of read and elevated temperature (Ei) Neces Es ctime un dependent. We Lever begins at different temperature for different material.

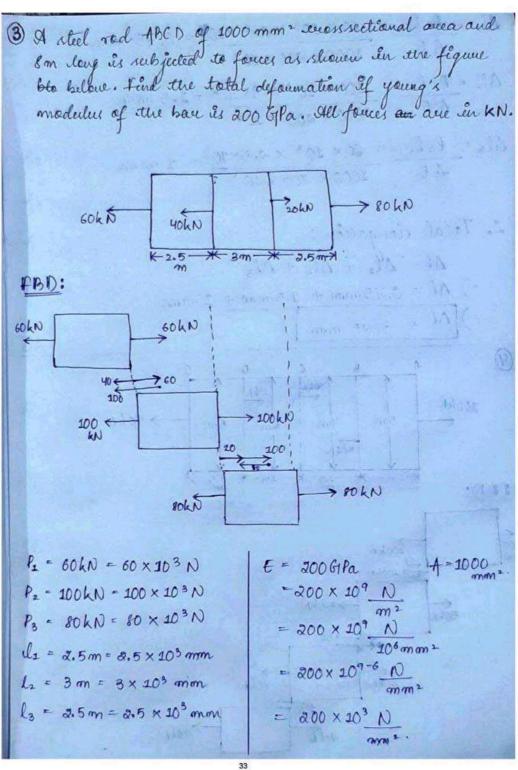




- > If the specimen is extended beyond the limit of proportionality my upto the point 'B', the material still remains elastic.
- > mut from 4 to B, stress-strain relation is not
- > The stress at 'B' Is called elastic limit.
- Again if the specimen is extended beyond the elastic
- → In the range of 'B' ito 'C' strain inverenses without inverence in stress.
- \* At point C' the material goes extended with decrease in read and the stress at point C is called upper-yield point.
- > At point D' the naterial again offers resistance to queater extension and the stress convergending to this point is called clower-yield point.
- → As the load is inversed, the extension inverses and the point 't' inclicates the niching of the specimen and the stress converponding to this point is called <u>ultimate</u> tendle stress.
- → Ms the extension is increased, the road required decuraces and the specimen breaks at the point of 'F' and this point is called sleers failure.







$$Al_{1} = \frac{P_{1} l_{1}}{A E} = 60 \times 10^{3} \times 3.5 \times 10^{3} = 0.75 \text{ mm}$$

$$Al_{2} = \frac{P_{1} l_{2}}{A E} = \frac{100 \times 10^{3} \times 3 \times 10^{3} = 1.5 \text{ mm}}{1000 \times 300 \times 10^{3}}$$

$$Al_{3} = \frac{P_{3} l_{3}}{A E} = \frac{80 \times 10^{3} \times 3.5 \times 10^{3} = 1 \text{ mm}}{4 E}$$

$$Al_{3} = \frac{P_{3} l_{3}}{1000 \times 300 \times 300 \times 10^{3}} = 1 \text{ mm}$$

$$Al_{4} = \frac{Al_{1} + Al_{2} + Al_{3}}{1000 \times 300 \times 10^{3}} = 1 \text{ mm}$$

$$Al_{5} = \frac{Al_{1} + Al_{2} + Al_{3}}{1000 \times 300 \times 10^{3}} = 1 \text{ mm}$$

$$Al_{1} = \frac{Al_{1} + Al_{2} + Al_{3}}{1000 \times 300 \times 10^{3}} = 1 \text{ mm}$$

$$Al_{2} = \frac{Al_{1} + Al_{2} + Al_{3}}{1000 \times 300 \times 10^{3}} = 1 \text{ mm}$$

$$Al_{1} = \frac{Al_{1} + Al_{2} + Al_{3}}{1000 \times 300 \times 10^{3}} = 1 \text{ mm}$$

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$$Al_{3} = \frac{Al_{1} + Al_{2} + Al_{3}}{1000 \times 300 \times 10^{3}} = 1 \text{ mm}$$

$$Al_{4} = \frac{Al_{1} + Al_{2}$$

$$P_{1} = 100 \text{ kN} = 100 \times 10^{3} \text{ N}$$

$$P_{2} = 50 \text{ kN} = 50 \times 10^{3} \text{ N}$$

$$P_{3} = 80 \text{ kN} = 80 \times 10^{3} \text{ N}$$

$$P_{4} = 90 \text{ kN} = 90 \times 10^{3} \text{ N}$$

$$P_{4} = \frac{1}{4} (5)^{2} = 19.63 \text{ m}^{2}$$

$$P_{4} = \frac{1}{4} (4)^{2} = 12.56 \text{ m}^{2}$$

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$$P_{4} = \frac{1}{4} (5)^{2} = 19.63 \text{ m}^{2}$$

$$P_{5} = \frac{1}{4} (5)^{2} = 19.63 \text{ m}^{2}$$

$$P_{7} = \frac{1}{4} (5)^{2} = 19.63 \text{ m}^{2}$$

$$P_{8} = \frac{1}{4} (5)^{2} = 19.63 \text{ m}^{2}$$

$$P_{9} = \frac{1}{4} (5)^{2} = 19.63 \text{ m}^{2}$$

$$P_{1} = \frac{1}{4} (5)^{2} = 19.63 \text{ m}^{2}$$

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$$P_{2} = \frac{1}{4} (5)^{2} = 19.63 \text{ m}^{2}$$

$$P_{3} = \frac{1}{4} (5)^{2} = 19.63 \text{ m}^{2}$$

$$P_{4} = \frac{1}{4} (5)^{2} = 19.63 \text{ m}^{2}$$

$$P_{5} = \frac{1}{4} (5)^{2} = 19.63 \text{ m}^{2}$$

$$P_{7} = \frac{1}{4} (5)^{2} = 19.63 \text{ m}^{2}$$

$$P_{1} = \frac{1}{4} (5)^{2} = 19.63 \text{ m}^{2}$$

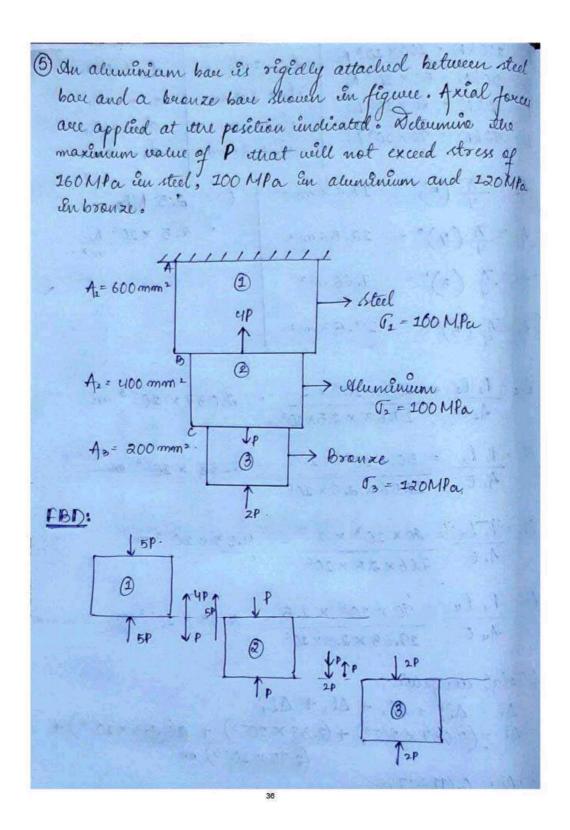
$$P_{2} = \frac{1}{4} (5)^{2} = 19.63 \text{ m}^{2}$$

$$P_{3} = \frac{1}{4} (5)^{2} = 19.63 \text{ m}^{2}$$

$$P_{4} = \frac{1}{4} (5)^{2} = 19.63 \text{ m}^{2}$$

$$P_{5} = \frac{1}{4} (5)^{2} = 19.63 \text{ m}^{2}$$

$$P_{7} = \frac{1}{4} (5)^{2} = 19.63 \text{$$



Fau section (2): A

$$T_{2} = \frac{P_{2}}{A_{2}}$$
=)  $100 = P_{3} = 100 \times 400$ 

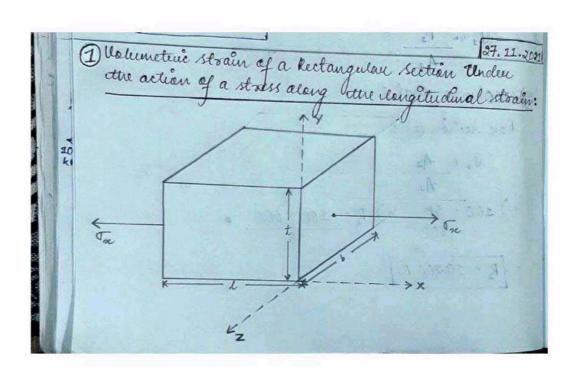
=)  $P_{2} = 40000 \text{ N}$ 

Fou section (3):

$$T_{3} = \frac{P_{3}}{A_{3}}$$
=)  $100 = \frac{2P}{200} = P_{5} = 100 \times 200$ 

=)  $P_{3} = 12000 \text{ N}$ 

E) washer with



let il, b, t auc ittre length, bueaden and ithickness of the rectangular block. Tx = itensele stuces un x - direction E = Young's Modulus μ= Paissen's ratio = - latinal strain Mongitudinal strain Mengitudinal strain: Cm = Tre -) ey = - m. (2) Similarly, \( \ell\_z = - \mu \overline{\tau}\_{\tau} \overline{\tau} But we have that,

we know that,

velume of a rectangular bettech is given by:

$$V = l \times b \times t$$

Now, derivating both the rides:

$$\frac{dv}{v} = \frac{cll}{l} + \frac{db}{b} + \frac{dt}{dt}$$

$$\frac{d}{v} = \frac{cll}{l} + \frac{db}{b} + \frac{dt}{dt}$$

$$\frac{d}{d} (l \times b \times t) + \frac{d}{d} (l \times b \times t) + \frac{d}{d} (l \times b \times t)$$

$$= \frac{dl}{l} + \frac{db}{b} + \frac{dt}{dt}$$

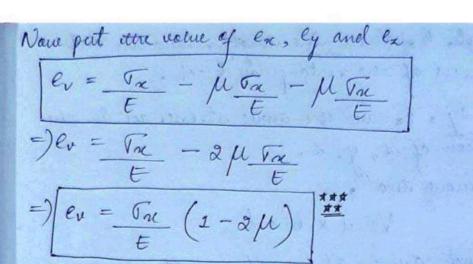
$$= \frac{dl}{l} + \frac{db}{l} + \frac{dt}{l}$$

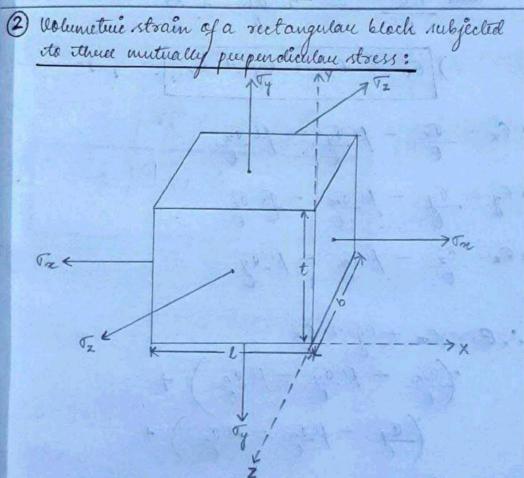
$$= \frac{dl}{l} = volumetaic strain$$

$$v$$

$$e_{n} = \frac{dl}{l} = v = \frac{dt}{t}$$

$$e_{y} = \frac{db}{b}$$





elet il, b, t aux the length, bueauth and thickness of the rectangular block. Tx, Ty, Tx and the atome stresses act in the direction of m, y, x. we know itrat. V= dx bxt. and du = dl + db + dt =) (ex = ex + ly + lz · la - Tx - My - Moz · ly = Ty - Mon - Moz · ez = oz - Mon - Moy :. eu = en + ey + ex = ( Ta - Moy - Moz + ) + ( Ty - 1150 - 1152 ) + E - Mon - Moy

=) 
$$ev = \frac{\sigma_{x}}{t} - \mu \frac{\sigma_{y}}{t} - \mu \frac{\sigma_{z}}{t} + \sigma_{y} - \mu \frac{\sigma_{x}}{t} - \mu \frac{\sigma_{z}}{t}$$

=)  $ev = \frac{1}{t} \left[ \frac{\sigma_{x}}{\tau_{x}} - \mu \frac{\sigma_{y}}{\tau_{z}} + \frac{\sigma_{y}}{\tau_{y}} - \mu \frac{\sigma_{x}}{\tau_{z}} - \mu \frac{\sigma_{z}}{\tau_{z}} - \mu \frac{\sigma_{z}}{\tau_{z}} \right]$ 

=)  $ev = \frac{1}{t} \left[ \frac{\sigma_{x}}{\tau_{x}} - \mu \frac{\sigma_{x}}{\tau_{y}} + \frac{\sigma_{y}}{\tau_{z}} - \mu \frac{\sigma_{y}}{\tau_{z}} + \frac{\sigma_{y}}{\tau_{z}} - \mu \frac{\sigma_{y}}{\tau_{z}} \right]$ 

=)  $ev = \frac{1}{t} \left[ \frac{\sigma_{x}}{\tau_{x}} - \mu \frac{\sigma_{x}}{\tau_{x}} + \frac{\sigma_{y}}{\tau_{y}} - \mu \frac{\sigma_{y}}{\tau_{z}} + \frac{\sigma_{z}}{\tau_{z}} - \mu \frac{\sigma_{z}}{\tau_{z}} \right]$ 

=)  $ev = \frac{1}{t} \left[ \frac{\sigma_{x}}{\tau_{x}} - \mu \frac{\sigma_{x}}{\tau_{x}} + \frac{\sigma_{y}}{\tau_{y}} - \mu \frac{\sigma_{y}}{\tau_{x}} + \frac{\sigma_{z}}{\tau_{z}} - \mu \frac{\sigma_{z}}{\tau_{z}} \right]$ 

=)  $ev = \frac{1}{t} \left[ \frac{\sigma_{x}}{\tau_{x}} - \mu \frac{\sigma_{x}}{\tau_{x}} + \frac{\sigma_{y}}{\tau_{x}} - \mu \frac{\sigma_{y}}{\tau_{x}} + \frac{\sigma_{z}}{\tau_{x}} - \mu \frac{\sigma_{y}}{\tau_{x}} + \frac{\sigma_{z}}{\tau_{x}} \right]$ 

=)  $ev = \frac{1}{t} \left[ \frac{\sigma_{x}}{\tau_{x}} - \mu \frac{\sigma_{x}}{\tau_{x}} + \frac{\sigma_{y}}{\tau_{x}} - \mu \frac{\sigma_{y}}{\tau_{x}} + \frac{\sigma_{z}}{\tau_{x}} - \mu \frac{\sigma_{y}}{\tau_{x}} + \frac{\sigma_{z}}{\tau_{x}} - \mu \frac{\sigma_{z}}{\tau_{x}} + \frac{\sigma_{z}}{\tau_{x}}$ 

## Complex Stress and Strain.

